

US EPA RECORDS CENTER REGION 5



487124

Ecology and Environment, Inc.

TDD# F5-8007-5A

Preliminary Hydrogeologic Report on the  
Federal Marine Terminals Property  
Riverview, Michigan

by Mark A. Hutson

In accordance with TDD# F5-8007-5A, Ecology and Environment, Inc. has completed an initial hydrogeologic field study of the Federal Marine Terminals property in Riverview, Michigan. Objectives of the study included identification of contaminants present in soils and ground, determination of groundwater flow characteristics, and evaluation of the potential for off-site migration of contaminants.

The property in question is an approximately 30 acre parcel along the Trenton Channel at the Detroit River. It is bounded on the east by the river, on the south by the Riverview boat dock, on the west by Jefferson Avenue, and on the north by the Firestone Steel plant (see locator map). Fill material was deposited on the site by unidentified parties over a period of many years. The exact time frame of filling operations is unknown but believed to be during the 1950's and early 1960's.

Contamination and buried steel drums were encountered by workers during the initial phase of site development for a facility planned by Federal Marine Terminals. Further development was stopped at that time and the site remains inactive to date.

The study, as authorized by the United States Environmental Protection Agency (USEPA), has consisted of three major components involving data collection on the property. These components included geophysical site investigation, soil boring and piezometer installation, and groundwater sampling.

#### Geophysical Testing

The geophysical testing portion of the study was subcontracted to Technos, Inc. Technos personnel utilized electromagnetic (EM) conductivity and magnetometer methods to characterize the site. EM was used to delineate areas of increased bulk ground conductivity possibly associated with concentrations of pollutants. The magnetometer was used to detect the presence of buried ferrous materials (i.e., steel drums).

### Geophysical Testing (continued)

Figure 1 shows the spatial distribution of magnetic anomalies across the site. As is depicted in this figure, the highest accumulation of buried ferrous materials exists in the northeast quadrant of the property. Fewer anomalies were detected across the central portion of the site. The southwest and western portions of the area showed few or no anomalies.

Figures 2A, 2B, and 2C are computer generated, 3-dimensional views of the sites showing relative conductivities of the materials present. Figures 3A and 3B are contour plots of the same data. As seen in these figures, the northeast and eastern portions of the site show significant increases in conductivity. According to Technos, "conductivities about 60 mm/m appear to be indicative of the clays present in the area". These conductivities found in background clays are nearly one order of magnitude less than the conductivities measured on the northeast portion of the site. Figure 3B magnifies areas along the Trenton Channel where areas of high conductivity meet the river.

With this information we were able to design our monitoring network to pick up the major areas of high conductivity while avoiding magnetic anomalies and the possibility of striking a buried metal object while drilling.

### Soil Boring and Piezometer Installation

In order to determine the geologic properties of the site and define the cause of the increased conductivities on site, a network of soil borings and piezometer installations was designed. Toledo Testing Laboratory, Inc. was contracted to perform the boring and well installation and also do soil testing. The network (see Plate 1) consisted of 19 borings into which piezometers were installed (see Diagram 1). Soil samples were taken using a standard split spoon sampler from which 8 soil samples were shipped for chemical analysis.

### Soil Boring and Piezometer Installation (continued)

Table 1 presents the results of sieve analysis performed on soil samples from borings 7, 10, and 18. Shelby tube samples of the underlying clay were obtained from borings #16, 17 and 19, and Table 2 presents the results of permeability tests which were run on these samples. As would be expected with filled areas, the composition of the soils varies greatly. However, the clay was observed to have a permeability of approximately  $2 \times 10^{-8}$  cm/sec in all three tested samples. All previously completed on-site soils investigations have shown the clay to be 30'-50' thick. In order to obtain a representative value of permeability of the fill material, in-situ falling head tests were performed in wells #3 and 7. These tests (see Appendix B) resulted in values of  $5 \times 10^{-5}$  cm/sec in well #7 and approximately  $3.5 \times 10^{-5}$  in well #3. Values in this range are normal for materials composed of silty sands<sup>2</sup>.

Logs of the soil borings (Appendix A) reveal a clay-fill interface surface as shown on Plate 2. Several of the borings penetrated a soft, black, organic layer at approximate elevation 573-574. As this elevation coincides with approximate river level and the lateral extent of this organic layer is relatively extensive, it is believed that this elevation represents the deepest extent of fill material. Sand and gravel deposits below the organics probably represents naturally deposited alluvial materials. The northwestward trending depression across the clay suggests the presence of the ancestral Monguagon Creek across the property at this location. Cross section A-A' and B-B' show the generalized subsurface profiles from the locations marked on Plate 1.

Plate 3 is a contour plot of the piezometric surface as defined by water level measurements taken on 2/24/81 and 2/27/81. As outlined in Appendix C, the volume of water flowing from the site into the Trenton Channel is approximately 56,000 gallons/year at an estimated velocity of 4 feet/year. It should be emphasized that these figures represent estimates based on the assumptions outlined in Appendix C. Additional groundwater flow is noted from the western portions of the fill toward the north and northeast. The relative elevations of the piezometric surface and river level suggest that at the time this data was collected,

### Soil Boring and Piezometer Installation (continued)

water was moving from the channel into the near stream alluvial deposits and fill material. This phenomena reinforces the suggestion of a positive link between the groundwater on the site and the river. Communication between the two will naturally result in occasional recharge of the groundwater in this manner.

### Conclusions

From the data which has been gathered to date, the geologic setting of the FMT property can be outlined. The entire site is underlain by a stiff clay layer which extends for 30'-50' below the fill and has a measured permeability on the order of approximately  $2 \times 10^{-8}$  cm/sec. This layer should be sufficient to prevent vertical migration of contaminants. The clay surface is overlain by sand and gravel deposits, some of which are probably naturally occurring alluvial deposits of the Trenton Channel or ancestral Monguagon Creek. The organic layer encountered in several borings probably represents the uppermost horizon of these alluvial deposits and marks the lowest extent of filled materials.

The soils encountered in the filled areas ranged from gravels to silty sands. Evaluation of falling head tests on two of the wells yielded values on the order of  $10^{-5}$  cm/sec. Horizontal movement of groundwater into the river will be approximately 0.1 gal/minute. At flow rates in this range, there is little possibility of detecting any contamination in the river. Flow from the western sections of the fill is in a northerly direction.

More information on the site will be available when chemical analysis of soil and water samples are received. At that time, this report will be updated to include that information.

### Recommendations

In order to ascertain the extent of contamination extending off-site in a northerly direction, additional boring and sampling would need to be completed.

If an absolute proof of communication between the river and groundwater is required, river and groundwater level recording devices will have to be installed on-site. The estimated cost of this would be approximately \$12,000 plus approximately 40 man-days for installation. An additional cost would be that required to send technicians to Detroit once a week for the duration of the records, (at least 6 months).

MH/df

#### REFERENCES

1 Technos, Inc., 1980, "Report of Geophysical Investigation at F.M.T., Firestone, and McLouth Steel Properties", Detroit, Michigan.

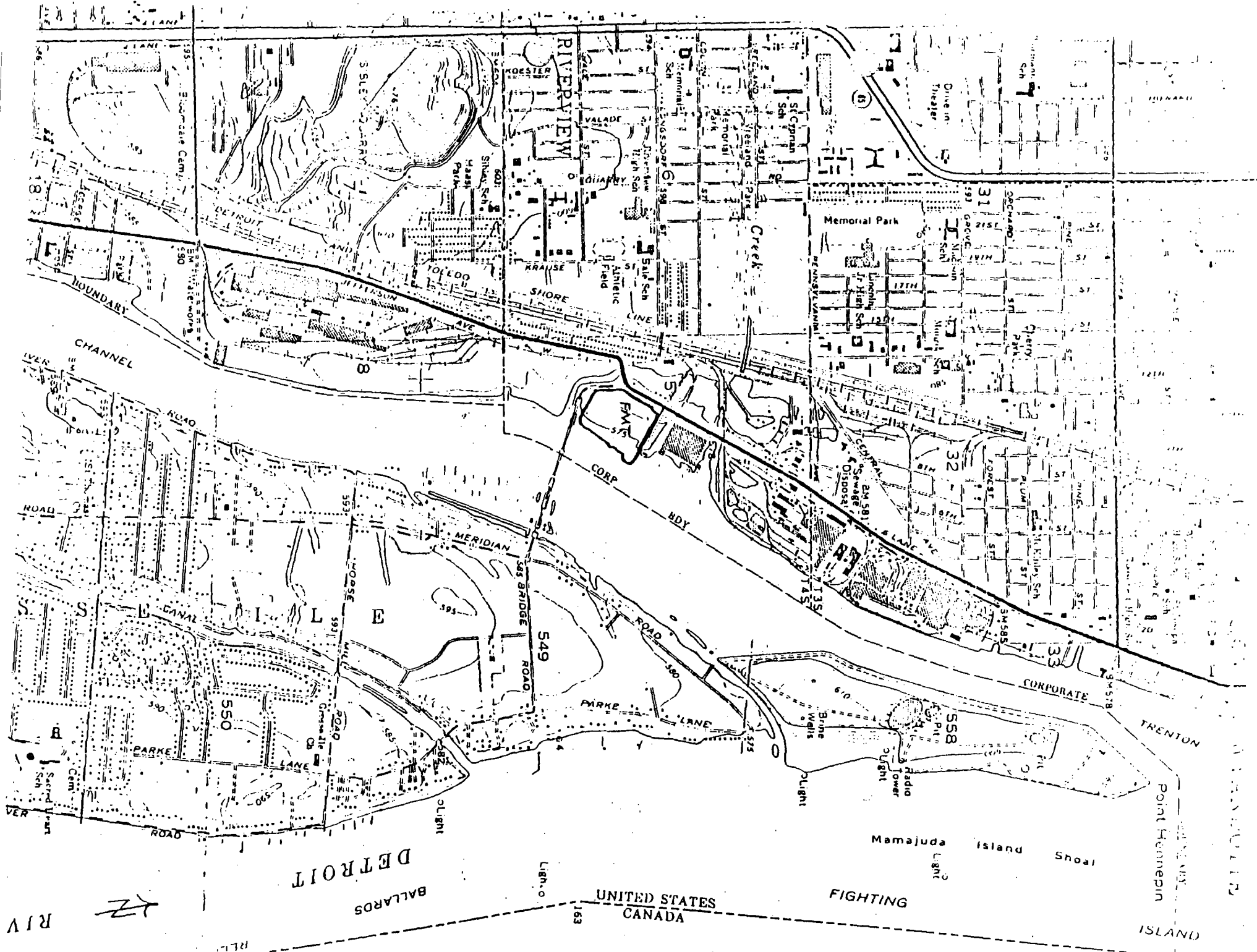
2 Freeze, R. Allan and Cherry, John A., 1979, "Groundwater", Prentice-Hall, Inc., Englewood Cliffs, N.J., p. 29

Dames and Moore, 1979, "Investigation of Potential Contamination - Firestone Site", Riverview, Michigan.

Applied Environmental Research, 1979, "Federal Marine Terminals, Inc. site Environmental Assessment", Riverview, Michigan.

Walton, W.C., 1970, Groundwater Resource Evaluation, McGraw Hill Book Company, p. 664

MH/df





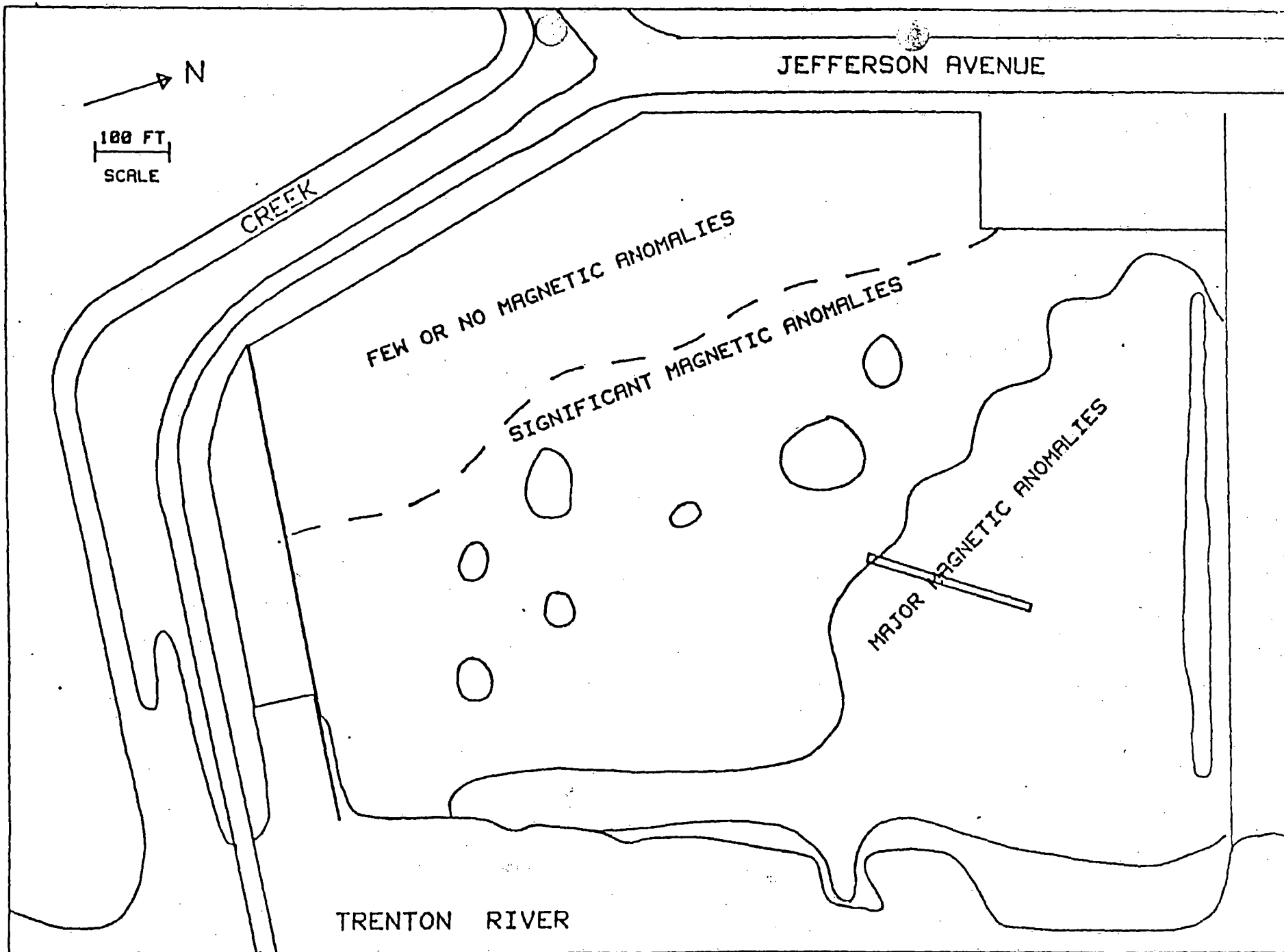


Figure 1 : F.M.T. Site; Magnetic Anomaly Distribution

Significant Anomalies — — — Major Anomalies —

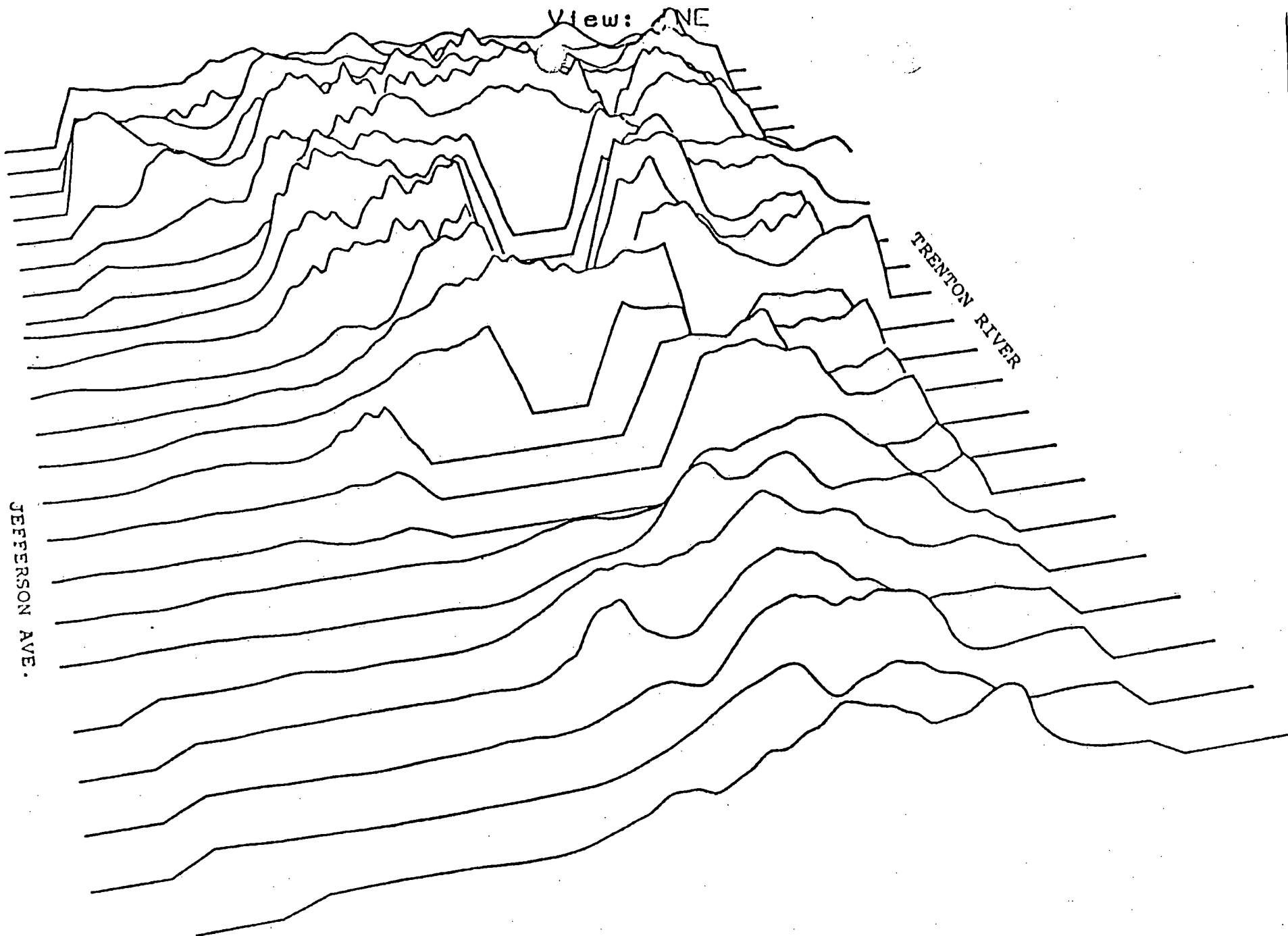


Figure 2A: F.M.T. Site; 3-Dimensional Conductivity Plot, northeast view.  
Figure is approximately to scale, 1000 by 1200 feet.  
GROUND CONDUCTIVITY

TECHNOS INC, MIAMI

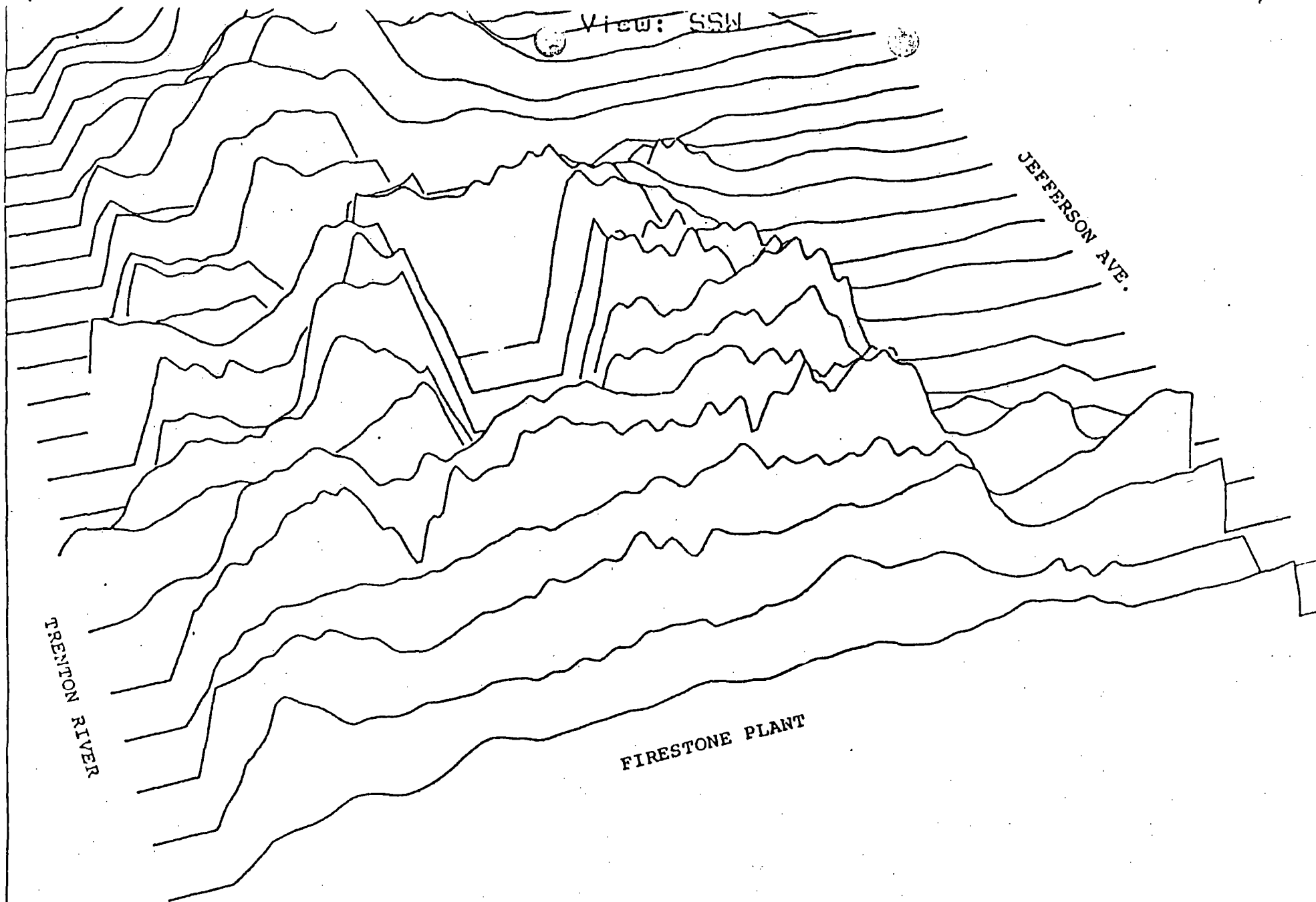


Figure 2B: F.M.T. Site; 3-Dimensional Conductivity Plot, south-southwest view.

Figure is approximately to scale, 100 by 1200 feet.

GROUND CONDUCTIVITY

TECHNOS INC, MIAMI

View: WNW

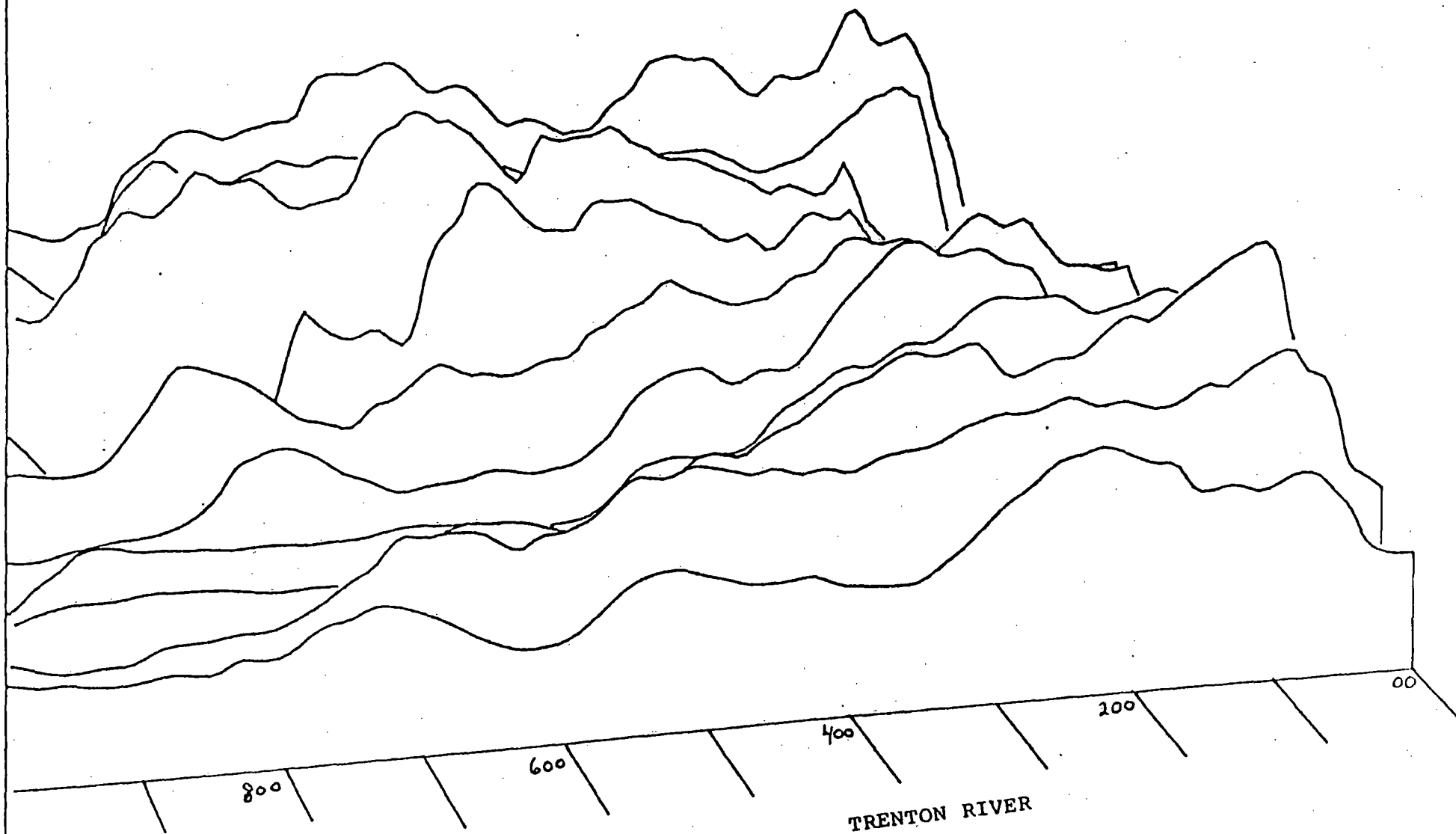


Figure 1C: F.M.T. Site; 3-Dimensional Conductivity Plot, Northeast corner.  
Indicated scale is in feet.

GROUND CONDUCTIVITY

TECHNOS INC, MIAMI.

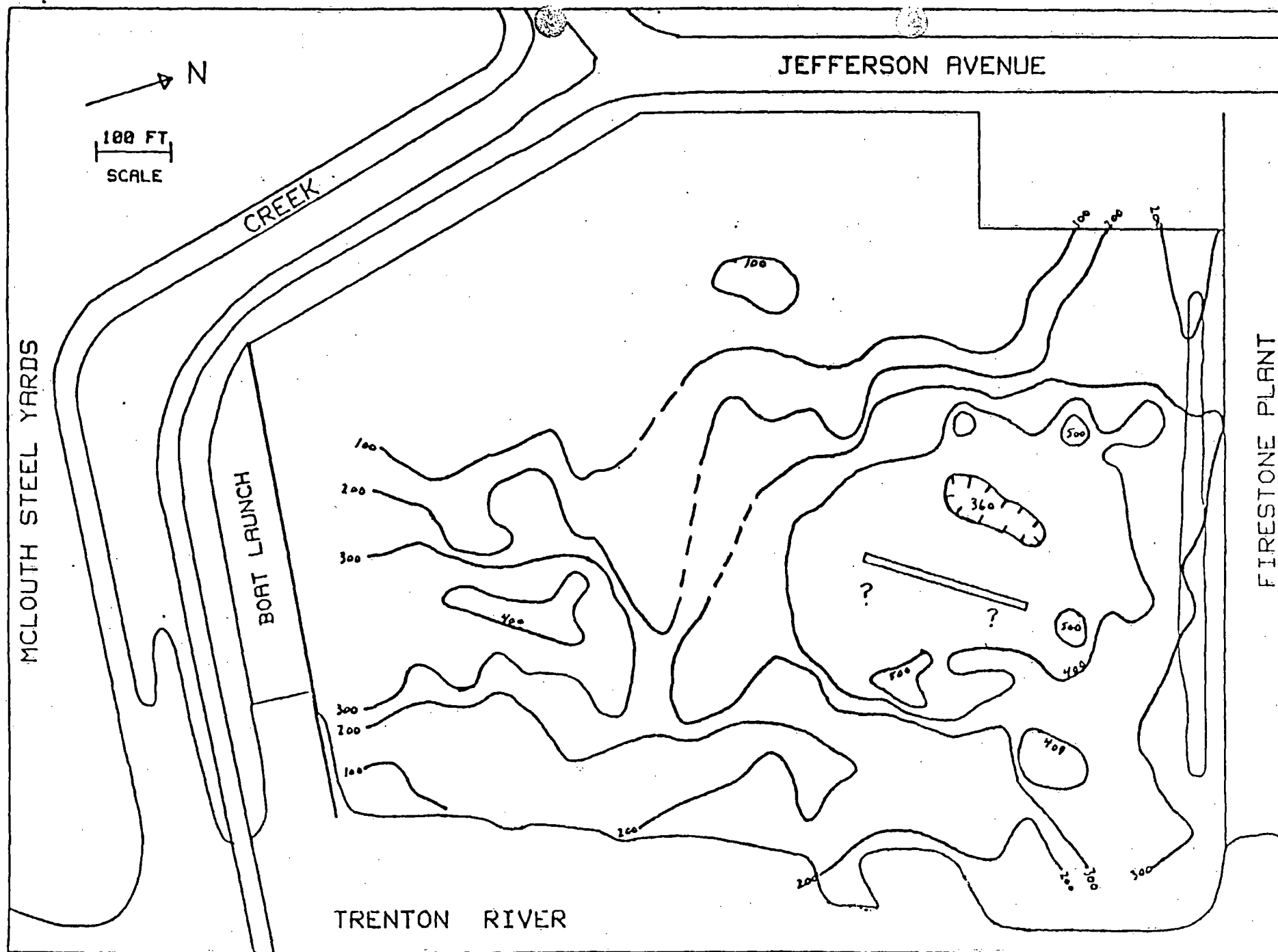


Figure 3A: F.M.T. Site; Generalized Ground Conductivity Contour Plot.

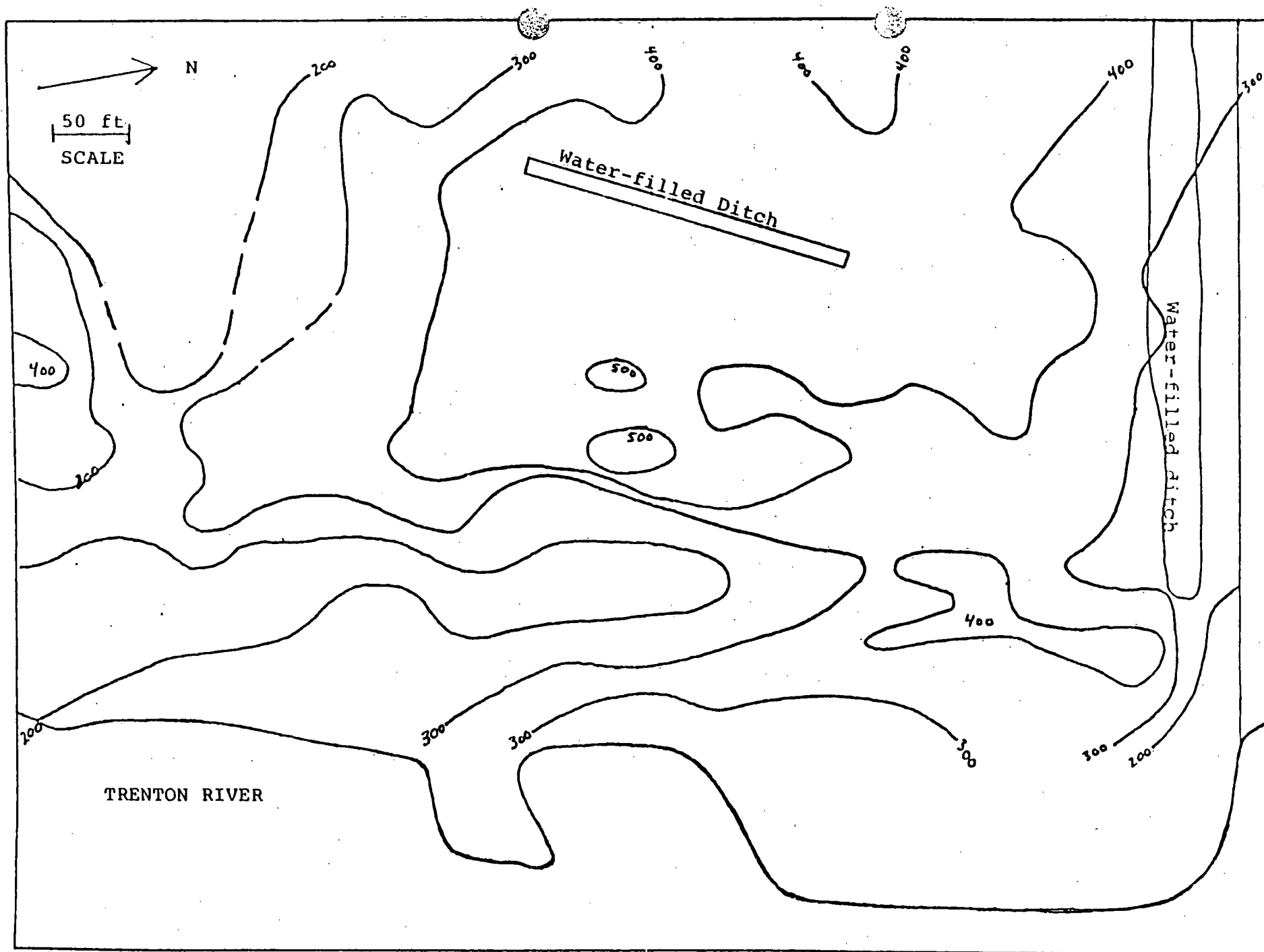
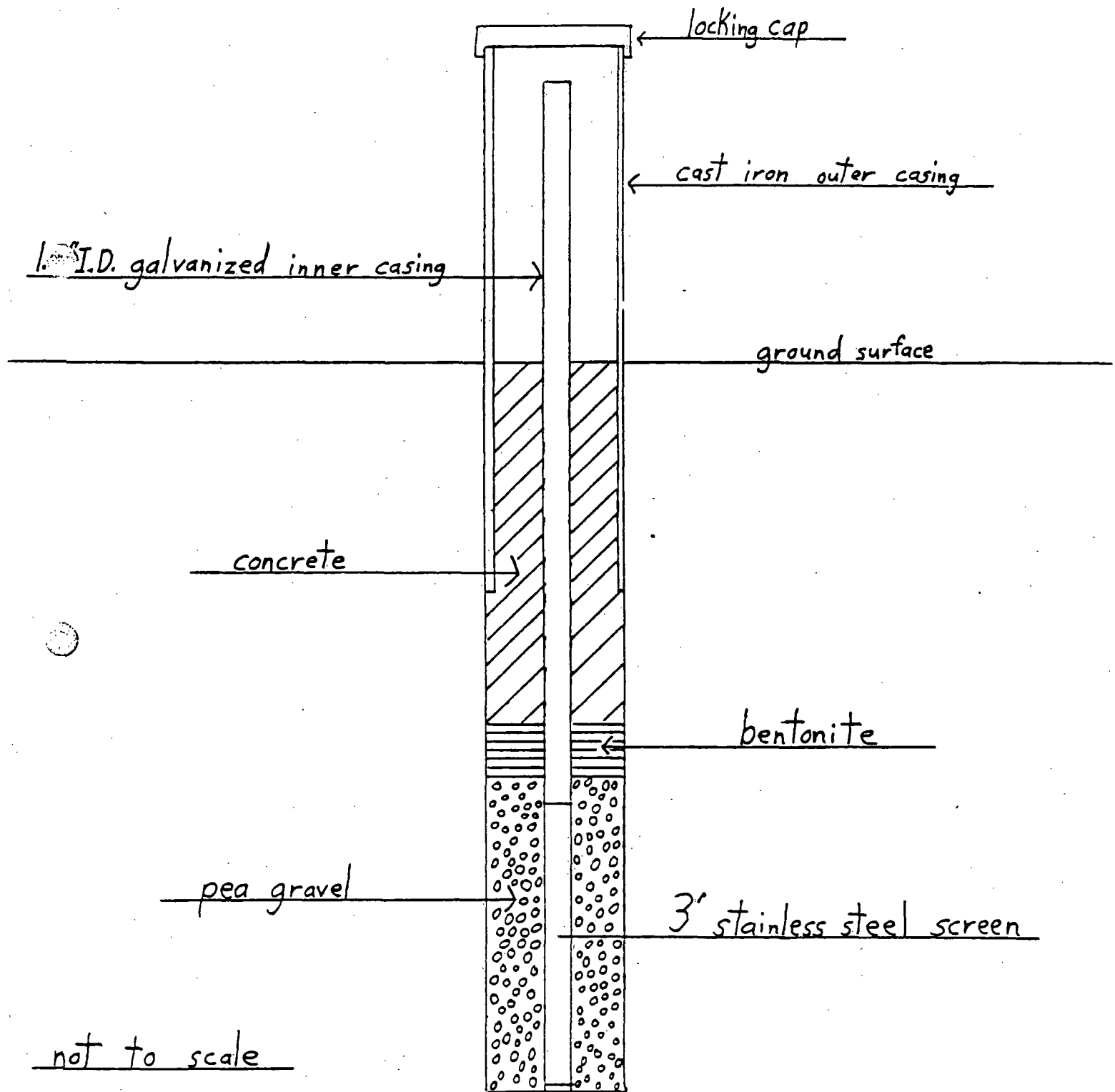


Figure 9B: F.M.T. Site; Generalized Ground Conductivity Contour Plot  
Northeast corner.

# Federal Marine Terminals





Toledo Testing Laboratory, Inc.  
Engineers • Chemists • Geologists

1810 North 12th Street  
Toledo, Ohio 43624

FEBRUARY 6, 1981

T.T.L. JOB NO. DR-4686

TABLE NO. 1

MECHANICAL ANALYSIS (SIEVE AND HYDROMETER) AND  
COMPOSITION OF SOIL

<u>BORING NUMBER</u>	<u>S I E V E   A N A L Y S I S</u>										
	<u>PERCENT PASSING SIEVE SIZES AND NUMBERS</u>										
	<u>1 1/2"</u>	<u>1"</u>	<u>3/4"</u>	<u>1/2"</u>	<u>3/8"</u>	<u>NO.4</u>	<u>NO.10</u>	<u>NO.20</u>	<u>NO.40</u>	<u>NO.100</u>	<u>NO.200</u>
7-A	100.00	100.00	100.00	100.00	100.00	99.91	99.45	99.36	99.24	77.63	53.0
10-B	100.00	100.00	100.00	100.00	100.00	99.47	98.25	97.55	97.08	42.86	21.0
18-D	100.00	90.66	86.91	80.76	75.46	63.51	47.49	39.03	33.77	26.99	22.0

COMPOSITION OF SOIL

<u>BORING NUMBER</u>	<u>GRAVEL (%)</u>	<u>SAND (%)</u>	<u>FINES</u>	
			<u>SILT (%)</u>	<u>CLAY (%)</u>
7-A	0.55	45.76	34.21	19.48
10-B	1.75	76.52	10.70	11.03
18-D	52.51	25.34	10.54	11.61



TABLE NO. 2

PERMEABILITY TEST

<u>BORING NUMBER</u>	<u>SAMPLE NUMBER</u>	<u>DEPTH (FT.-IN.)</u>	<u>NATURAL MOISTURE CONTENT (%)</u>	<u>COEFFICIENT OF PERMEABILITY (cm/sec)</u>
16	ST-1	4'4"-6'0"	15.4	$2.0 \times 10^{-8}$
17	C	14'0"-15'6"	15.5	$1.8 \times 10^{-8*}$
19	ST-1	5'9"-6'10"	18.4	$2.1 \times 10^{-8}$

\*Sample remolded and consolidated at the approximate overburden pressure  $\sigma_v = 1,500$  psf for 24 hours prior to test.

# SOIL BORING LOG

Toledo Testing Laboratory, Inc.

1810 North 12th Street

Toledo, Ohio 43624

(419) 241-7175

## Project

WELL INSTALLATION - RIVERVIEW, MICHIGAN

### Boring Location

Job No. DR-4686

Date JANUARY 14, 1981

### Salt Borin

[illegible]

### Type of Sample

A Auger (Disturbed)  
—Split Tube Sampling—  
H Thin-walled (House)  
Tube-Undisturbed  
J Jar-Disturbed  
ST Shelby Tube-Undisturbed  
RC Rock Core  
NR Indicates "No Recovery"

### Remarks

Total Footage: 5'0"  
Overburden Drilled: 5'0"  
Rock Cored: NONE  
Drillers: TK-TB-OF

### Groundwater Observations

At completion: 3'6" below the  
surface

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Project WELL INSTALLATION - RIVERVIEW, MICHIGAN

### Boring Location

Job No. DR-4686

Date JANUARY 15, 1981

Soll Boring No. 2

[illegible]

### Type of Sample

A Auger (Disturbed)  
 —Split Tube Sampling—  
 H Thin-walled (House) Tube-Undisturbed  
 J Jar-Disturbed  
 ST Shelby Tube-Undisturbed  
 RC Rock Core  
 NR Indicates "No Recovery"

### Remarks

Remarks: \_\_\_\_\_  
 Total Footage: 5'6"  
 Overburden Drilled: 5'6"  
 Rock Cored: NONE  
 Drillers: TK-TB-DF

### Groundwater Observations

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WELL INSTALLATION - RIVERVIEW, MICHIGAN

### Boring Location

Job No. DR-4686

Date JANUARY 15, 1981

**Soll Boring No.** 3

[illegible]

### Type of Sample

A Auger (Disturbed)  
 —Split Tube Sampling—  
 H Thin-walled (House) Tube-Undisturbed  
 J Jar-Disturbed  
 ST Shelby Tube-Undisturbed  
 RC Rock Core  
 NR Indicates "No Recovery"

### Remarks

Total Footage: 10' 6"  
Overburden Drilled: 10' 6"  
Rock Cored: NONE  
Drillers: TK-TB-DF

### Groundwater Observations:

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WELL INSTALLATION - RIVERVIEW, MICHIGAN

**Boring Location:**

Job No. DR-4686

Date JANUARY 15, 1981

**Soil Boring No.** 4

[illegible]

### Type of Sample

A Auger (Disturbed)  
 —Split Tube Sampling—  
 H Thin-walled (House)  
 Tube-Undisturbed  
 J Jar-Disturbed  
 ST Shelby Tube-Undisturbed  
 RC Rock Core  
 NR Indicates "No Recovery"

### Remarks

Remarks: \_\_\_\_\_  
 Total Footage: \_\_\_\_\_ 6'0"  
 Overburden Drilled: \_\_\_\_\_ 6'0"  
 Rock Cored: \_\_\_\_\_ NONE  
 Drillers: \_\_\_\_\_ TK-TB-DF

## Groundwater Observations



(419) 241-7175

Date JANUARY 15, 1981

[illegible]

-5-

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Project WELL INSTALLATION - RIVERVIEW, MICHIGAN

Boring Location \_\_\_\_\_ Job No. DR-4686

Job No. DR-4686

Date JANUARY 16, 1981

Soll Boring No. 6

[illegible]

### Type of Sample

**A** Auger (Disturbed)  
— Split Tube Sampling—  
**H** Thin-walled (Housel)  
Tube-Undisturbed  
**J** Jar-Disturbed  
**ST** Shelby Tube-Undisturbed  
**RC** Rock Core  
**NR** Indicates "No Recovery"

## Remarks

Total Footage: 6'0"  
 Overburden Drilled: 6'0"  
 Rock Cored: NONE  
 Drillers: TK-TB-DF

### Groundwater Observations

# SOIL BORING LOG

## Toledo Testing Laboratory, Inc.

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### Project

WELL INSTALLATION - RIVERVIEW, MICHIGAN

### Boring Location

Job No. DR-4686

Date JANUARY 16, 1981

Soil Boring No. 7[illegible]

### Type of Sample

A Auger (Disturbed)  
 —Split Tube Sampling—  
 H Thin-walled (House)  
 Tube-Undisturbed  
 J Jar-Disturbed  
 ST Shelby Tube-Undisturbed  
 RC Rock Core  
 NR Indicates "No Recovery"

### Remarks

Total Footage: 10' 6"  
Overburden Drilled: 10' 6"  
Rock Cored: NONE  
Drillers: TK-TB-DF

### Groundwater Observations





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**Project.**

WELL INSTALLATION - RIVERVIEW, MICHIGAN

### Boring Location

Job No. DR-4686

Date JANUARY 16, 1981

Soll Boring No. 8

**Type of Sample**  
**A Auger (Disturbed)**  
**— Split Tube Sampling—**  
**H Thin-walled (House)**  
**Tube-Undisturbed**  
**J Jar-Disturbed**  
**ST Shelby Tube-Undisturbed**  
**RC Rock Core**  
**NR Indicates "No Recovery"**

### Remarks

Total Footage: 7'0"

Overburden Drilled: 7'0"

Rock Cored: NONE

Drillers: TK-TB-OF

### Groundwater Observations

# SOIL BORING LOG

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**Project.**

WELL INSTALLATION - RIVERVIEW, MICHIGAN

### Boring Location

Job No. DR-4686

Date JANUARY 16, 1981

Soil Boring No. 9[illegible]

### Type of Sample

A Auger (Disturbed)  
 —Split Tube Sampling—  
 H Thin-walled (Housel)  
 Tube-Undisturbed  
 J Jar-Disturbed  
 ST Shelby Tube-Undisturbed  
 RC Rock Core  
 NR Indicates "No Recovery"

### Remarks

Total Footage: 6'0"  
Overburden Drilled: 6'0"  
Rock Cored: NONE  
Drillers: TK-TB-DF

## Groundwater Observations

# SOIL BORING LOG

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**Project.**

WELL INSTALLATION - RIVERVIEW, MICHIGAN

### Boring Location

Job No. DR-4686

Date JANUARY 21, 1981

Soil Boring No. 10

[illegible]

### Type of Sample

A Auger (Disturbed)  
 - Split Tube Sampling -  
 H Thin-walled (House)  
 Tube-Undisturbed  
 J Jar-Disturbed  
 ST Shelby Tube-Undisturbed  
 RC Rock Core  
 NR Indicates "No Recovery"

### Remarks

Total Footage: 15'6"  
Overburden Drilled: 15'6"  
Rock Cored: NONE  
Drillers: TK-TB-DF

## Groundwater Observations

# SOIL BORING LOG

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Project WELL INSTALLATION - RIVERVIEW, MICHIGAN

### Boring Location

Job No. DR-4686

Date JANUARY 21, 1981

Soll Boring No. 11

[illegible]

### e of Sample

Auger (Disturbed)  
Split Tube Sampling—  
Thin-walled (Housel)  
Tube-Undisturbed  
Bar-Disturbed  
Housel Tube-Undisturbed  
Rock Core  
Indicates "No Recovery"

### Remarks

Total Footage: 8'6"  
Overburden Drilled: 8'6"  
Rock Cored: NONE  
Drillers: TK-TB-DF

### Groundwater Observations

**Environmental Sustainability**

# SOIL BORING LOG

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### Project.

WELL INSTALLATION - RIVERVIEW, MICHIGAN

### Boring Location

Job No. DR-4686

Date JANUARY 21, 1981

Soil Boring No. 12

[illegible]

### Type of Sample

A Auger (Disturbed)

—Split Tube Sampling—

H Thin-walled (House)

**Tube-Undisturbed**

**J Jar-Disturbed**

**ST Shelby Tube-Undisturbed**

AC Rock Core

NR Indicates "No Recovery"

### Remarks

Total Footage: 6'0"

Overburden Drilled: 6'0"

Rock Cored: NONE

Drillers: TK-T8-DF

## Groundwater Observations

# SOIL BORING LOG

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Project WELL INSTALLATION - RIVERVIEW, MICHIGAN

### Boring Location

Job No. DR-4686

Date JANUARY 21, 1981

Soil Boring No. 13

[illegible]

### Type of Sample

A Auger (Disturbed)  
 - Split Tube Sampling -  
 H Thin-walled (House) Tube-Undisturbed  
 J Jar-Disturbed  
 ST Shelby Tube-Undisturbed  
 RC Rock Core  
 NR Indicates "No Recovery"

### Remarks

Total Footage: 8'6"  
Overburden Drilled: 8'6"  
Rock Cored: NONE  
Drillers: TK-TB-DF

### Groundwater Observations

# SOIL BORING LOG

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Project WELL INSTALLATION - RIVERVIEW, MICHIGAN

**Boring Location:**

Job No. DR-4686

JANUARY 21, 1981

Date \_\_\_\_\_

Soll Boring No. 14

[illegible]

### Type of Sample

A Auger (Disturbed)  
—Split Tube Sampling—  
H Thin-walled (Housel)  
Tube-Undisturbed  
J Jar-Disturbed  
ST Shelby Tube-Undisturbed  
RC Rock Core  
NR Indicates "No Recovery"

### Remarks

Total Footage: 6'0"  
Overburden Drilled: 6'0"  
Rock Cored: NONE  
Drillers: TK-TB-DF

### Groundwater Observations

# SOIL BORING LOG

## Toledo Testing Laboratory, Inc.

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Project WELL INSTALLATION - RIVERVIEW, MICHIGAN

### Boring Location

Job No. DR-4686

Date JANUARY 21, 1981

Soll Boring No. 15

[illegible]

### Type of Sample

A Auger (Disturbed)  
— Split Tube Sampling —  
H Thin-walled (Housel)  
Tube-Undisturbed  
J Jar-Disturbed  
ST Shelby Tube-Undisturbed  
AC Rock Core  
NR Indicates "No Recovery"

### Remarks

Total Footage: 6'0"  
Overburden Drilled: 6'0"  
Rock Cored: NONE  
Drillers: TK-TB-DF

## Groundwater Observations





# SOIL BORING LOG

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Project WELL INSTALLATION - RIVERVIEW, MICHIGAN

### Boring Location

Job No. DR-4686

Date JANUARY 22, 1981

Soil Boring No. 17

[illegible]

### Type of Sample

A Auger (Disturbed)  
—Split Tube Sampling—

H Thin-walled (Housel)  
Type-Uncut

↓ Jar-Disturbed

ST Shelby Tube-Undisturbed

AC Rock Corp

NR Indicates "No Recovery"

### Remarks

Total Footage: 18'0"

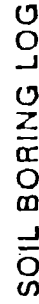
Overburden Drilled: 18'0"

Rock Cored: NONE

Drillers: TK-TB-DF

### Groundwater Observations

\_\_\_\_\_



1810 North 12th Street  
Toledo, Ohio 43624  
(419) 241-7175

11

# SOIL BORING LOG

## Toledo Testing Laboratory, Inc.

1810 North 12th Street  
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Project WELL INSTALLATION - RIVERVIEW, MICHIGAN

### Boring Location

Job No. DR-4686

Date JANUARY 22, 1981

Soll Boring No. 19

[illegible]

### Type of Sample

A Auger (Disturbed)  
—Split Tube Sampling—  
H Thin-walled (House)  
Tube-Undisturbed  
J Jar-Disturbed  
ST Shelby Tube-Undisturbed  
RC Rock Core  
NR Indicates "No Recovery"

**Remarks**

Total Footage: 7'0"  
Overburden Drilled: 7'0"  
Rock Cored: NONE  
Drillers: TK-TB-DF

## Groundwater Observations

T (minutes)

Well "3" (K 1)

$$K = \frac{r^2 \ln(L/r)}{2L T_0}$$

$$= \frac{(106)^2 \ln(3/106)}{(2)(3)(34)}$$

$$= 383 \times 10^{-5} \text{ 1/secs}$$

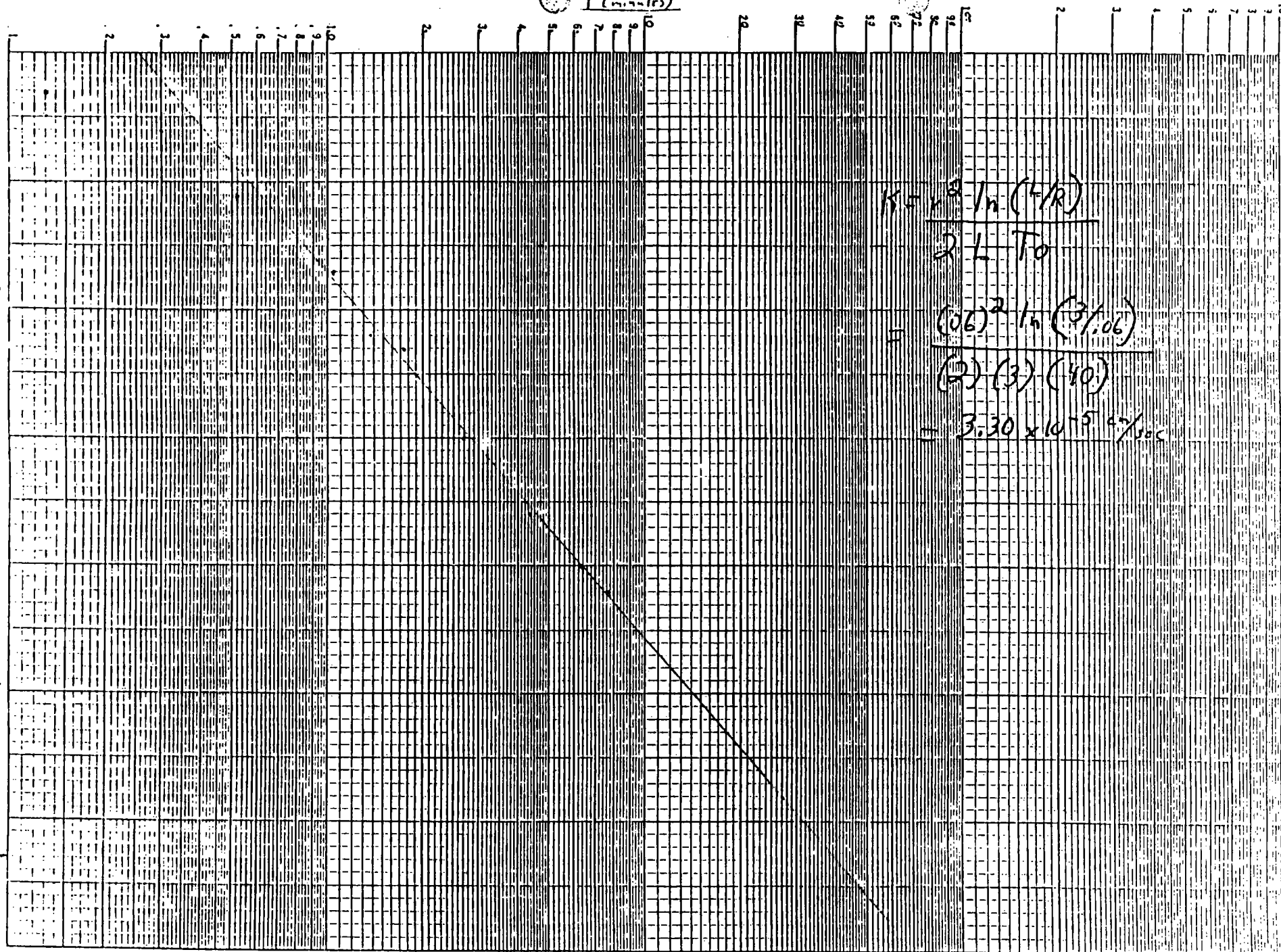
T<sub>0</sub> = 34 minutes

Appendix B

Well #3

Run #2

T (minutes)



$$K = \frac{r^2 \ln(r/R)}{2L T_0}$$

$$= \frac{(0.6)^2 \ln(3/0.6)}{(2)(3)(40)}$$

$$= 3.30 \times 10^{-5} \text{ cm/sec}$$

$T_0 = 40 \text{ minutes}$

T (minutes)

$$K = \frac{r^2 \ln \left( \frac{4}{\pi} \right)}{2 L T_0}$$

$$= \frac{(66)^2 \ln \left( \frac{3}{0.1} \right)}{(2) (3) (25.8)}$$

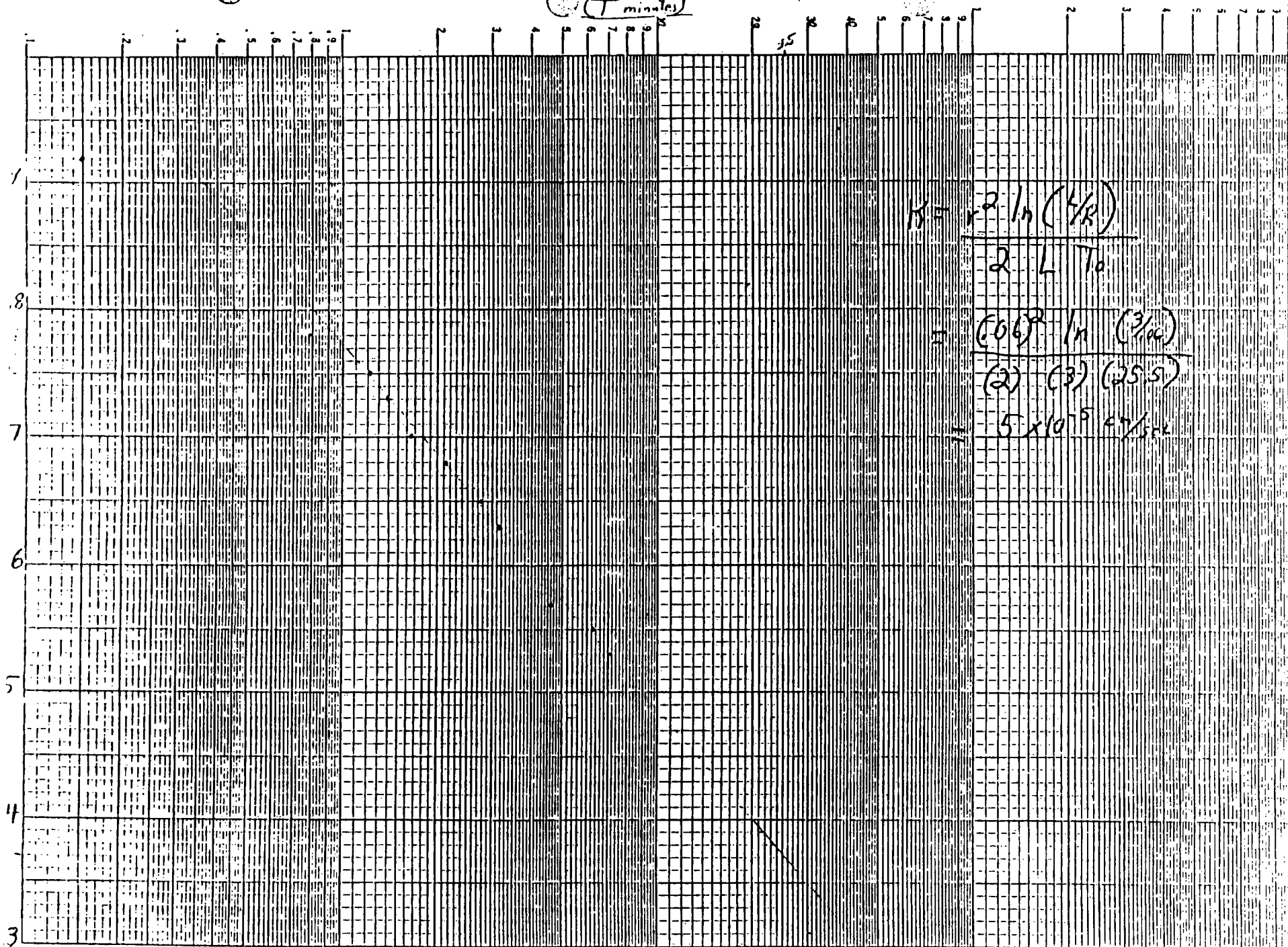
$$= 5 \times 10^{-5} \text{ sec}^{-1}$$

$T_0 = 25.8 \text{ minutes}$

Appendix B

Well 17 Run 2

(T minutes)



$$K = \frac{r^2 \ln \left( \frac{4}{r} \right)}{2 L T_0}$$

$$= \frac{(0.6)^2 \ln \left( \frac{3}{0.6} \right)}{(2) (3) (25.5)}$$

$$= 5 \times 10^{-5} \text{ ft/sec}$$

$$T_0 = 25.5 \text{ minutes}$$



## APPENDIX C

The volume of water discharged from the groundwater to the Trenton Channel of the Detroit River can be estimated using Darcy's Law:

$Q = -KIA$  where,

$Q$  = volume of water,  $\text{ft}^3/\text{yr}$ .

$K$  = hydraulic conductivity,  $\text{cm}/\text{sec}$  or  $\text{ft}/\text{yr}$

$I$  = hydraulic gradient

$A$  = area through which groundwater discharge occurs,  $\text{ft}^2$

$V$  = specific discharge

$n_e$  = effective porosity

### Assumptions:

$K = 4 \times 10^{-5} \text{cm}/\text{sec}$  or  $40 \text{ ft}/\text{yr}$ .

$I = .015$

$A = 12 \text{ ft} \times 1100 \text{ ft} = 13200 \text{ ft}^2$

$n_e = 15\%$

### Therefore:

$Q = 40 \text{ ft}/\text{yr} \times .015 \times 13200 \text{ ft}^2$

$= 7920 \text{ ft}^3/\text{yr}$ . or approx. 59,000 gal/yr.

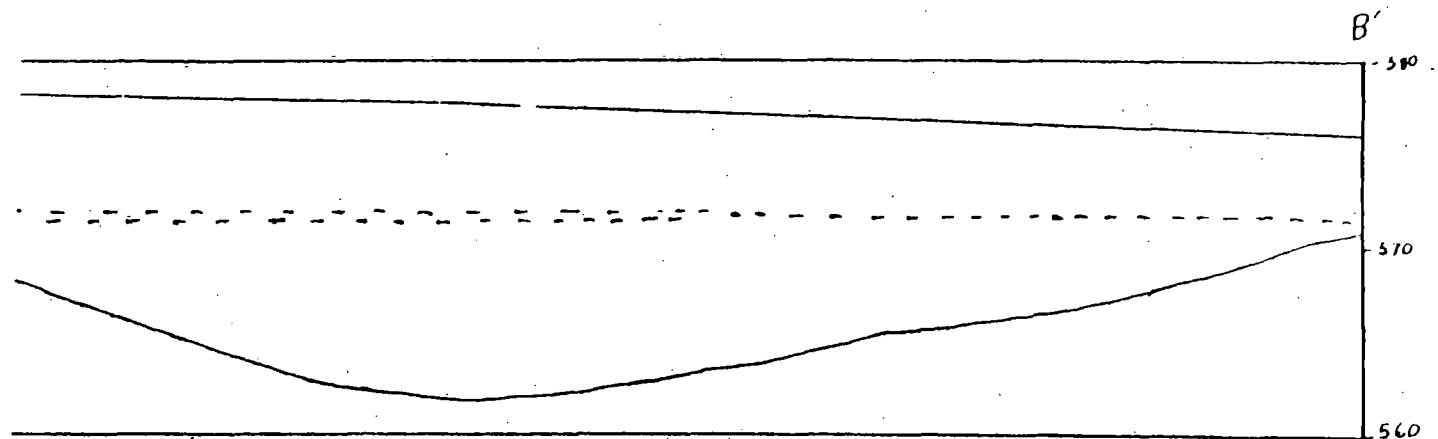
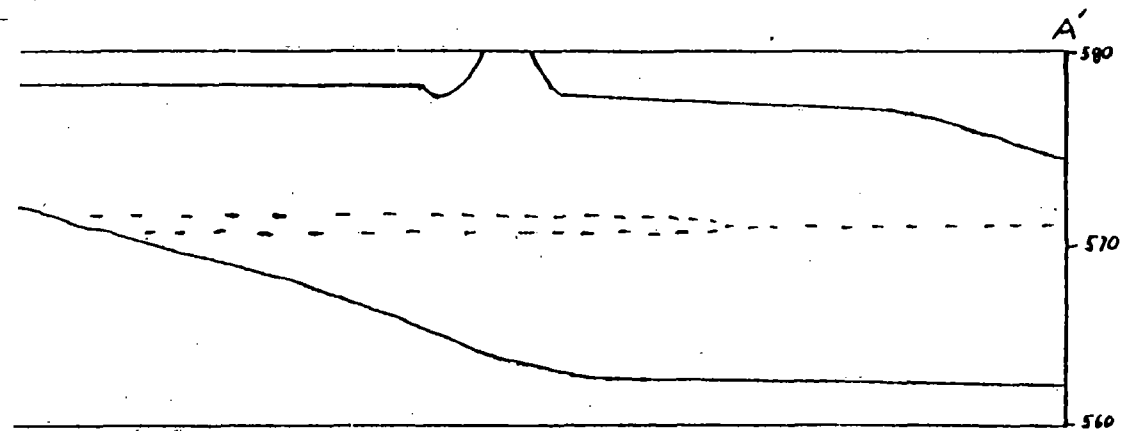
To estimate the velocity that water is moving toward the channel we calculated the specific discharge using the same assumptions:

$$V = -KI \frac{1}{n_e}$$

$V = .40 \text{ ft}/\text{yr} \times .015 \times 6.66$

$V = 4 \text{ ft}/\text{yr}$ .

These figures represent what is probably a worst case estimate due to the fact that the gradient becomes less in the northeast corner of the porerty. Also, since the water level measurments from which this data is generated were taken in the spring, the total cross sectional area of the saturated zone above the clay is probably at or near it's greatest size.



Vertical Scale 1"=10'  
Horizontal Scale 1"=100'

Federal Marine Terminals  
Riverview, Michigan